

## Some considerations on TOF-NSE

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Recently a future plan of a huge spallation neutron source has been proposed in a framework of the Japan Hadron Project (JHP), in which accelerated protons with 100-200  $\mu\text{A}$  and 1-2 GeV will be used for the production of neutrons. Here, as a new concept, a unique cold moderator is considered, which can produce high intense pulsed-cold-neutrons with the extreme wide burst-width. If it will be realized, it will confer benefits on elastic scattering TOF-instruments, such as SAN in KENS, which does not require high time-resolution. However, it is a "devil" for ordinary inelastic scattering TOF-spectrometers with high energy-resolution, such as LAM in KENS. In these inelastic spectrometers, high time-resolution is required and the energy-resolution is approximately given by  $2(\text{burst-width})/(\text{time-of-flight})$ . It means that the ordinary inelastic scattering spectrometer with  $\epsilon/E_i = 0.005$  must be constructed much farther from this moderator, at about 300 m.

Because the area of JHP is very small, it is hard to prepare such a long flight path. Even if it could be constructed with the long flight path, the available band-width of neutron wavelength becomes very small. For our future plan, many attempts should be performed to "invent" a new type of the TOF-spectrometer, which can realize the high energy-resolution even in the condition of a short distance and a wide burst-width on various spectrometers, including the ordinary one.

The TOF spin-echo method (TOF-NSE) is one candidate for these trials. The pure spin-echo method<sup>[1]</sup> has been already realized on the steady state sources, and many low energy excitations in magnetic systems, polymers and so on, have been observed. TOF-NSE was proposed by Mezei in 1979<sup>[2]</sup> but not still realized at the spallation neutron sources. At KENS, we constructed a test machine of TOF-NSE in 1983.

If incident polarized neutrons with velocity  $V_1$  is used in NSE, the polarization observe dby the analyzer,  $P(V_1)$ , can be written as

$$P(V_1) = \int d\epsilon S(\epsilon) \cos(\omega_1 t_1 - \omega_2 t_2), \quad (1)$$

where  $\epsilon = m(V_1^2 - V_2^2)/2$ ,  $t_1 = l_1/V_1$ ,  $t_2 = l_2/V_2$  and  $\omega_{1,2} = \gamma H_{1,2}$ .  $m$  is the neutron mass,  $H_{1,2}$  a magnetic field in precession section I and II, and  $V_2$  is the velocity of scattered neutrons.  $S(\epsilon)$  is a scattering function of a sample. If  $V_1 - V_2 \ll V_1$  and  $l = l_1 = l_2$  and  $H = H_1 = H_2$ , Eq.(1) is written as

$$P(V_1) = \int d\epsilon S(\epsilon) \cos(\tau\epsilon) = S'(\tau), \quad (2)$$

where  $\tau = \gamma l / (mV_1^3) \cdot H$ . In principle, it is possible to measure  $S'(\tau)$  in two kinds of neutron sources; the steady state source and the pulsed source. In the case of the steady state source,  $\tau$  can be represented as a function of  $H$  because of  $V_1 = \text{constant}$ , and  $S'(\tau)_{\text{steady}}$  can be observed by changing magnetic field  $H$ . In the case of the pulsed source, pulsed white neutrons are used as incident neutrons. Here,  $V_1$  is determined as  $V_1 = L/t$  and  $\tau$  can be written as  $\tau = \gamma H l / (mL^3) \cdot t^3$ , where  $L$  is the total flight-path length and  $t$  the time-of-flight. This means  $S'(\tau)_{\text{TOF}}$  can be automatically observed as a function of  $t^3$  in the constant magnetic field  $H$ . This is a most useful nature of TOF-NSE.

A schematic layout of TOF-NSE is shown in Fig.1. Here we assume that  $\pi$ -turner and  $\pi/2$ -turners perfectly work for every neutron velocity, and that  $l_3 = l_4 = l_5 = l_6 = l_7 = 0$  and  $\delta l_0 = 0$  in order to simplify the equation. The observed TOF-spectrum,  $I(t)$ , is written as

$$I(t) = 1/2 \int P^t P_1^l P_2^l P_1^\omega P_2^\omega \delta(t - t_0 - t_1 - t_2) (1 + \cos(\omega_1 t_1 - \omega_2 t_2)) \\ S(\epsilon) \delta(E_i - E_f - \epsilon) dt_0 dt_1 dt_2 d\omega_1 d\omega_2 d\epsilon. \quad (3)$$

Here,  $P_{1,2}^l$  and  $P_{1,2}^\omega$  represent are fluctuations of the lengths and the precession frequency in precession sections ( $i = 1,2$ ), respectively.  $E_i$  and  $E_f$  are incident and scattered neutron energies, respectively.  $P^t$  is a pulse shape function of the neutron burst. Let's represent  $P_{1,2}^l$ ,  $P_{1,2}^\omega$  and  $P^t$  by Gaussian as

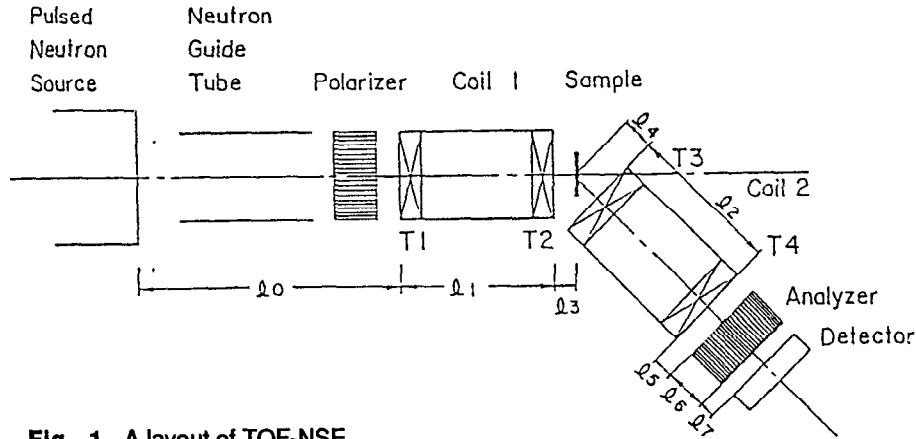


Fig. 1 A layout of TOF-NSE.

$$P^t = (\sqrt{2\pi}\sigma_t)^{-1} \exp(-(t_0 - t_0^0)^2 / 2\sigma_0^2), \quad (4)$$

$$P_{1,2}^\omega = (\sqrt{2\pi}\sigma_{\omega_{1,2}})^{-1} \exp(-(\omega_{1,2} - \omega_{1,2}^0)^2 / 2\sigma_{\omega_{1,2}}^2) \quad (5)$$

and

$$P_{1,2}^l = (\sqrt{2\pi}\sigma_{l_{1,2}})^{-1} \exp(-(l_{1,2} - l_{1,2}^0)^2 / 2\sigma_{l_{1,2}}^2), \quad (6)$$

where  $t_0^0$ ,  $\omega_{1,2}^0$  and  $l_{1,2}^0$  are mean values of  $t_0$ ,  $\omega_{1,2}$  and  $l_{1,2}$ .  $\sigma_0$  corresponds to the neutron burst-width. If  $\sigma_{l_{1,2}}/V_1 \ll \sigma_0$ ,  $I(t)$  can be written as

$$I(t) = (2\sqrt{2\pi}\sigma_0)^{-1} \int dt_0 d\epsilon \exp(-(t - t_0^0 - t_1^0 - t_2^0)^2 / 2\sigma_0^2) \\ [1 + \Psi(a_1, a_2)\Phi(a_1, a_2)] S(\epsilon) \delta(E_i - E_f - \epsilon). \quad (7)$$

Here,

$$\Psi(a_1, a_2) = a_1 a_2 / \sqrt{(a_1^2 + g_1^2 h_1^2)(a_2^2 + g_2^2 h_2^2)} \\ \cdot \exp(-(g_1^2 + h_1^2)/(a_1^2 + g_1^2 h_1^2) + (g_2^2 + h_2^2)/(a_2^2 + g_2^2 h_2^2)) \quad (8)$$

and

$$\Phi(a_1, a_2) = \cos(a_1/(a_1^2 + g_1^2 h_1^2) - a_2/(a_2^2 + g_2^2 h_2^2)) \tag{9}$$

where  $t_0^0 = l_0/V_1$ ,  $a_i = V_i/\omega_i^0 l_i^0 = 1/\omega_i^0 t_i^0$ ,  $g_i = \sigma_i^l/l_i^0$  and  $h_i = \sigma_i^w/\omega_i^0$ .

$\Psi(a_1, a_2)$  and  $\Phi(a_1, a_2)$  are a damping factor and an oscillation factor, respectively. Since  $V_1 \sim V_2$ ,  $\Psi(a_1, a_2)$  is described by

$$\Psi(a_1, a_2) = \Psi_g(a_1) = a_1^2/(a_1^2 + g^4) \exp(-2g^2/(a_1^2 + g^4)). \tag{10}$$

where  $g = g_1 = g_2 = h_1 = h_2$  is assumed in order to simplify.  $\Psi_g(a_1)$  was calculated as a function of  $H \cdot l$  in the case of  $\lambda_1 = 9 \text{ \AA}$ , and is shown in Fig.2. Here,  $\lambda_1$  is a wavelength of incident neutron. Furthermore  $\Psi_g(a_1)$  was calculated as a function of  $\lambda_1$  in the case of  $H \cdot l = 120 \text{ Oe}$ , and is shown in Fig.3. If  $g > 10^{-4}$ ,  $\Psi_g(a_1)$  goes down drastically as  $\lambda_1$  or  $H \cdot l$  increase. These results indicate  $g < 10^{-4}$  is required to obtain a good neutron economy. In the same assumption, the oscillation factor  $\Phi$  is described by

$$\Phi(a_1, a_2) = \Phi_g(a_1, a_2) = \cos(a_1/(a_1^2 + g^4) - a_2/(a_2^2 + g^4)). \tag{11}$$

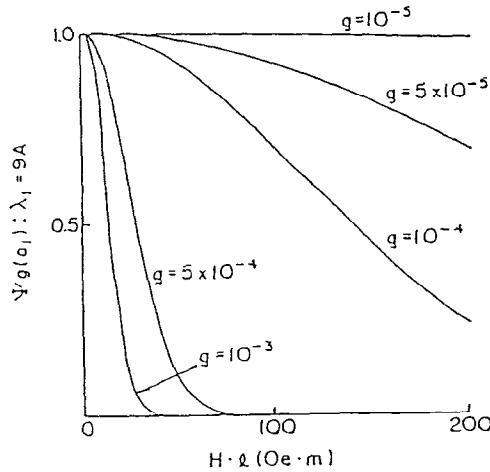
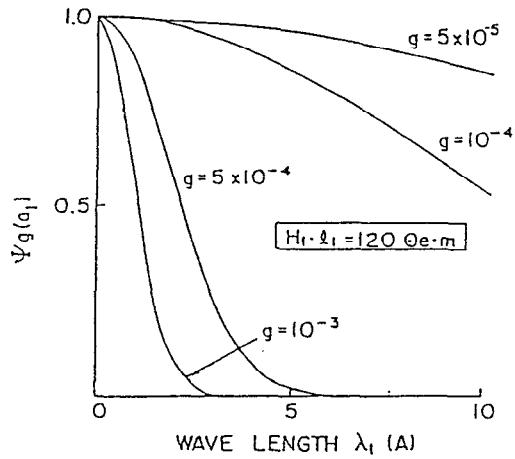
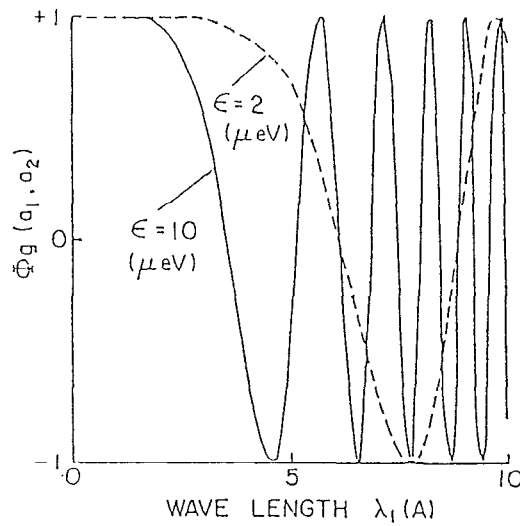


Fig. 2 Damping factor  $\Psi_g$  and  $H \cdot l$ . The solid lines are calculated with  $\lambda_1 = 9 \text{ \AA}$ .



**Fig. 3** Damping factor  $\Psi_g$  and wavelength  $\lambda_1$ . The solid lines are calculated with  $H \cdot l = 120 Oe \cdot m$ .

In the case of  $S(\epsilon) = (\delta(\epsilon - \epsilon_0) + \delta(\epsilon + \epsilon_0))/2$ ,  $H \cdot l = 120 Oe \cdot m$  and  $g = 10^{-4}$ ,  $\Phi_g(a_1, a_2)$  was calculated with  $\epsilon_0 = 2 \mu eV$  and  $\epsilon_0 = 10 \mu eV$  and shown in Fig.4. This results show the oscillation of  $\Phi_g(a_1, a_2)$  with  $\epsilon > 2 \mu eV$  can be observed in the range  $2.5 \text{ \AA} < \lambda_1 < 10 \text{ \AA}$ .



**Fig. 4** Oscillation factor  $\Phi_g$  and wavelength  $\lambda_1$ . The solid line is calculated with  $\epsilon = 10 \mu eV$  and  $H \cdot l = 120 Oe \cdot m$ . The dashed line is calculated with  $\epsilon = 2 \mu eV$  and  $H \cdot l = 120 Oe \cdot m$ .

The effect of the burst-width on the TOF-NSE should be discussed using Eq.(7). As is obvious from this equation, if the burst-width is much smaller than a period of  $\Phi_g$  one can expect no effects on TOF-NSE spectrum. Since  $\Psi_g$  changes very slowly under  $g = 10^{-4}$  as shown in Figs.2 and 3, it is possible to consider that  $\Psi_g$  is not affected by the burst-width. In order to observe a clear oscillation of  $S'(\tau)_{TOF}$  under  $l_0 = 18m$  and  $0 < \lambda_1 < 9A$ , the following condition is at least required:

$$3\epsilon\omega l \cdot (burst - width)/(2l_0 \cdot 1000) \sim 0.1 \ll 1 \quad (12)$$

In the case of  $(burst - width) \sim 200\mu sec$  (KENS-I) and  $H \cdot l = 120Oe \cdot m$ , the 'no effect' can be realized in the range  $\epsilon < 17\mu eV$ . Under these results, our test machine was designed with  $g \sim 10^{-4}$  and  $H \cdot l = 120Oe \cdot m$ . It is shown by the photograph (see Fig.5). In the case of  $(burst - width) \sim 1000\mu sec$  (JHP) and  $H \cdot l = 120Oe \cdot m$ , one can observe the clear oscillation only in the range  $\epsilon < 3\mu eV$ . These results indicate that the TOF-NSE spectrum is much affected by the burst-width and can give correct information on  $S(\epsilon)$  only in very small range. If one constructs TOF-NSE under the wide burst-width, the complete determination of many parameters mentioned above and the precise data correction will be necessary.

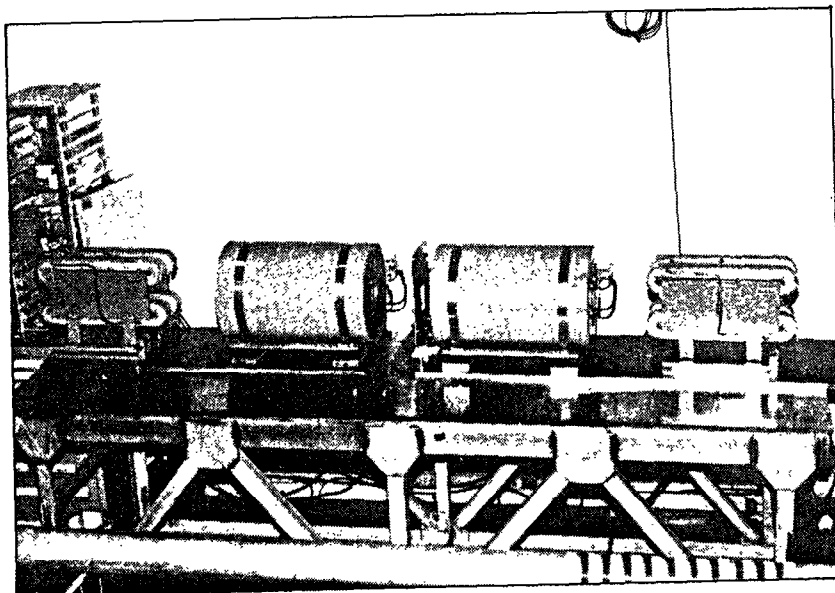


Fig. 5 Photograph of the test machine.

### References

1. F. Mezei, *Z. Physik* **255** (1976) 146.
2. F. Mezei, *Nucl. Instru. Methods* **164** (1979) 153.